

① Summit Curve \Rightarrow

\rightarrow Upward Gradient is followed by Downward Gradient

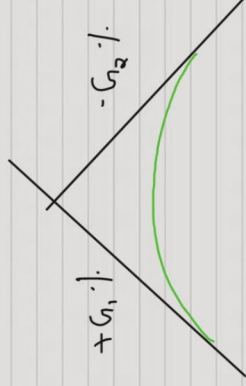
Area and Volume - Part I

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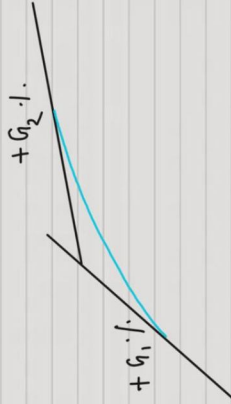
U/w Gr. = +ve
D/w Gr. = -ve

Net change in Gradient

$$G_1 = |G_1 - (-G_2)| \%$$



\rightarrow Steeper U/w Gr. is followed by milder U/w Gr.



$$G_1 = |G_1 - G_2| \%$$

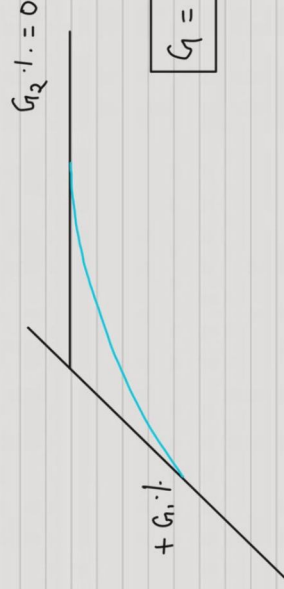
\rightarrow Milder U/w Gr. is followed by steeper U/w Gr.



$$G_1 = |G_1 - (-G_2)| \%$$

$$G_1 = |G_2 - G_1| \%$$

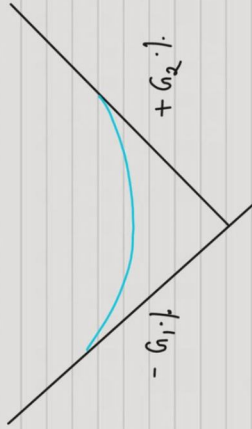
\rightarrow U/w Gr. followed by Flat Ground profile \Rightarrow



$$G_1 = |G_1 - 0|$$

② Valley Curve (sag curve) ⇒

→ Downward Gradient is followed by Upward Gradient -



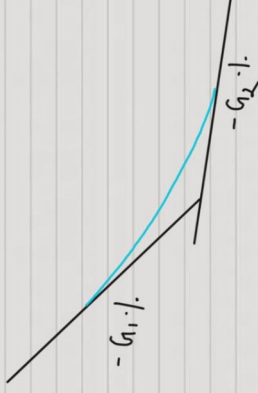
u/w Gr. = +ve
D/w Gr. = -ve

Net change in Gradient

$$G = |-G_1 - (+G_2)| \%$$

$$G = |-(G_1 + G_2)| \%$$

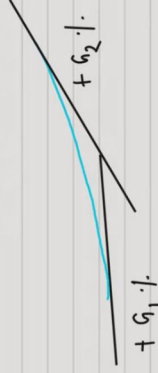
→ Steeper D/w Gr. is followed by milder D/w Gr.



$$G = |-G_1 - (-G_2)| \%$$

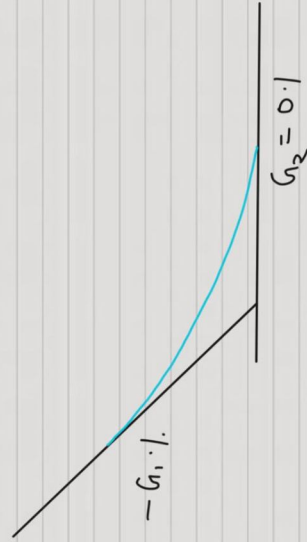
$$G = |(G_2 - G_1)| \%$$

→ Milder v/w Gr. is followed by steeper v/w Gr.



$$G = |G_1 - G_2| \%$$

→ Flat Ground profile ⇒



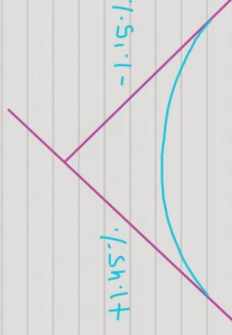
$$G = |-G_1| \%$$

Q. → A vertical curve has an u/w Gr. of +1.45% which is followed by a down Gr. of -1.15%. The rate of change of Gradient is 0.35% per chain length of 20m. Determine length of vertical curve.

Sol. ⇒

$$G = |1.45 - (-1.15)| \%$$

$$G = 2.6 \%$$



0.35 % of change of Gradient — 20m.

$$1 \text{ %} \rightarrow \frac{20}{0.35}$$

$$2.6 \text{ %} \rightarrow \frac{20}{0.35} \times 2.6$$

$$L = \frac{148.57 \text{ m.}}{}$$

Q. → A vertical curve has an upw Gr. of +1.45%. which is followed by a down Gr. of -1.15%. The rate of change of gradient is 0.35% per chain length. Determine length of vertical curve.

solⁿ = Δ

$$G_1 = |1.45 - (-1.15)| \text{ %}$$

$$G_1 = 2.6 \text{ %}$$

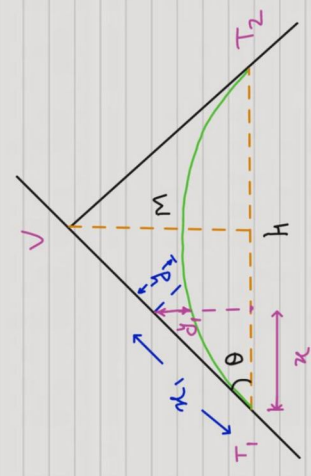
$$0.35 \text{ %} \rightarrow 1 \text{ chain length}$$

$$1 \text{ %} \rightarrow \frac{1 \text{ chain length}}{0.35}$$

$$2.6 \text{ %} \rightarrow \frac{1 \text{ chain length} \times 2.6}{0.35}$$

$$L = 7.428 \text{ chain}$$

Assumption on vertical curve →



- ① $T_1H = L/2$
- ② $VM = MH$
- ③ $T_1V = T_1M = T_1H$

④ offsets from tangent T_1, V are proportional to square of distance from T_1 .

$$y \propto x_1^2$$

Since curve is flat so we can say

$$y_1 \propto x_1^2$$

First

$$\cos \theta = \frac{x}{x_1}$$

$$x_1 = x \sec \theta$$

$$RL_{a'} = RL_a - y_1$$

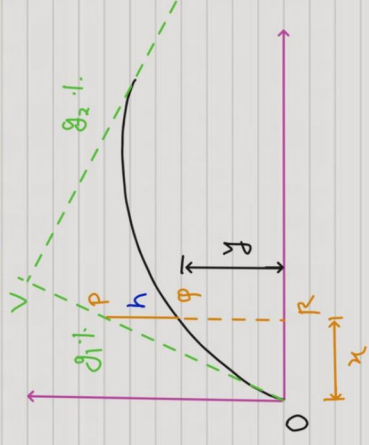
$$RL_a = RL_{T_1} + \frac{g_1}{100} \times x_1$$

$$RL_{a'} = \left[RL_{T_1} + \frac{g_1}{100} \times x_1 \right] - \left[\left(\frac{x_1}{x} \right)^2 \times y_1 \right]$$

Similarly

$$RL_{b'} = RL_b - y_2$$

Tangent Connection Method \Rightarrow



$$h \propto x^2$$

$$h = Cx^2$$

Equation of Parabola

$$y = ax^2 + bx + c$$

from eqⁿ of parabola

$$y \propto x^2$$

$$h \propto x^2$$

$$h = Cx^2 \longrightarrow \textcircled{i}$$

$$x = 0, \frac{dy}{dx} = g_1 \%$$

$$b = g_1$$

Difference in elevation betⁿ a vertical curve & tangent to it varies as a square of horizontal distance from the point of tangency/curve.

This difference in elevation is called tangent constⁿ.

from eqⁿ of parabola

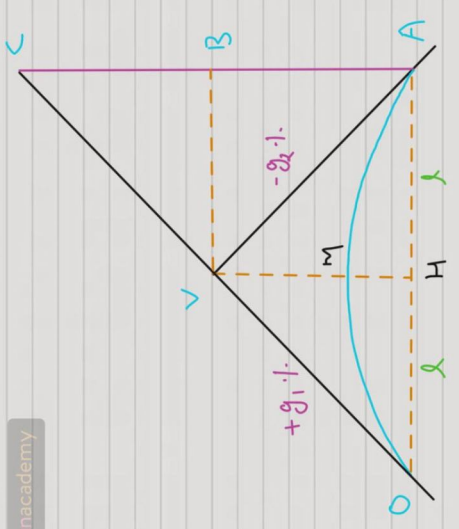
$$y \propto x^2$$

$$h \propto x^2$$

$$h = Cx^2 \longrightarrow \textcircled{i}$$

$$x = 0, \frac{dy}{dx} = g_1 \%$$

$$b = g_1$$



Extend OV line to OC such that $OV = VC$
 & it is observed that point C vertically above A.

$$AC = AB + BC \quad \rightarrow \quad (2)$$

$$BC = VH$$

$$g_1 \cdot l = \frac{VH}{l}$$

$$BC = VH = g_1 \cdot l$$

Similarly $AB = -g_2 \cdot l$

from eq. (2)

$$AC = (g_1 - g_2) l \quad \rightarrow \quad (3)$$

Q. 3.1. Rising Gradient meets a 2.1. Down Gradient. A vertical curve 200m. long is to be used. The pegs are to be fixed at 20m. Interval. Calculate the elevation of Curve point by tangent connection method. RL of apex - 350m & change - 1000m.

from eq. (1)

$$h = C \pi^2$$

$$AC = C (2l)^2$$

$$\frac{AC}{4l^2} = C$$

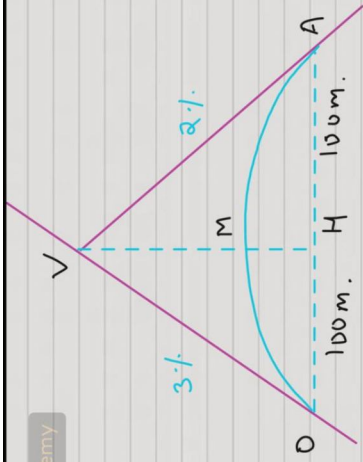
from eq. (3)

$$C = \frac{(g_1 - g_2) l}{4l^2}$$

$$C = \frac{(g_1 - g_2)}{4l}$$

Solⁿ =

$$\text{Curve length} = 200\text{m.}$$



$$OM = \frac{OA}{2} = \frac{200}{2} = 100\text{m.}$$

$$OH = OM = OV = 100\text{m.}$$

$$\text{Change of } \theta = 1000 - 100 = 900\text{ m.}$$

$$\text{Change of } A = \text{Change of } \theta + \text{Curve length} \\ = 900 + 200 = 1100\text{ m.}$$

$$\text{Peg Interval} = 20\text{m.}$$

$$\text{No. of Stations} = \frac{200}{20} = 10 \text{ stations}$$

No. of Station on each side of apex = 5

$$\text{RL of Station } O = RL_V - \frac{3}{100} \times 100 \\ = 350 - 3 = 347\text{ m.}$$

$$\text{RL of Station } A = RL_V - \frac{2}{100} \times 100 \\ = 350 - 2 = 348\text{ m.}$$

$$C = \frac{(g_1 - g_2)}{4L}$$

$$C = \frac{0.03 - (-0.02)}{4 \times 100} = 1.25 \times 10^{-4}$$

$$h = Cx^2$$

$$h_1 = 1.25 \times 10^{-4} \times 20^2 = 0.05\text{ m.}$$

$$h_2 = 1.25 \times 10^{-4} \times 40^2 = 0.2\text{ m.}$$

$$h_3 = 1.25 \times 10^{-4} \times 60^2 = 0.45\text{ m.}$$

$$h_4 = 1.25 \times 10^{-4} \times 80^2 = 0.8$$

$$h_5 = 1.25 \times 10^{-4} \times 100^2 = 1.25$$

$$h_6 = 1.25 \times 10^{-4} \times 120^2 = 1.8$$

$$h_7 = 1.25 \times 10^{-4} \times 140^2 = 2.45$$

$$h_8 = 1.25 \times 10^{-4} \times 160^2 = 3.2$$

$$h_9 = 1.25 \times 10^{-4} \times 180^2 = 4.05$$

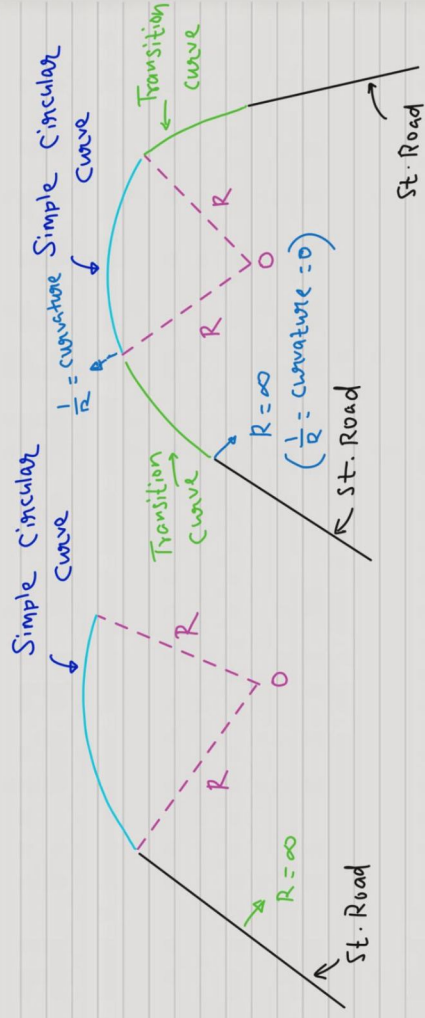
$$h_{10} = 1.25 \times 10^{-4} \times 200^2 = 5$$

Station	Chainage	Grade elevation	Tangent Connection	Curve elevation
0	900	347	0	347
1	920	347.6	0.05	347.55
2	940	348.2	0.2	348
3	960	348.8	0.45	348.35
4	980	349.4	0.8	348.6
5	1000	350	1.25	348.75
6	1020	350.6	1.8	348.8
7	1040	351.2	2.45	348.75
8	1060	351.8	3.2	348.6
9	1080	352.4	4.05	348.35
10	1100	353	5	348

Area and Volume - Part II

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Transition Curve \Rightarrow



\Rightarrow **Curve of variable radii** Introduce betⁿ a straight line and a simple circular curve.

- \rightarrow Transition Curve provides a gradual change from st. line to circular curve & from circular curve to st. line.
- \rightarrow It is tangential to st. line & also meets circular curve tangentially at the junction.
- \rightarrow It's curvature is zero ($R = \infty$) at junction with straight line & curvature is $\frac{1}{R}$ at the junction with simple circular curve.

\Rightarrow **Rate of increase of curvature** along the transition curve is equal to rate of increase of super-elevation.

\rightarrow The length of transition curve should be such that full super-elevation is achieved at the junction with circular curve.

Derivation of Ideal Transition Curve \Rightarrow

Centrifugal force (P) should increase uniformly with distance from beginning of transition curve.

$$P \propto l \quad \rightarrow \quad (1)$$

$P =$ Centrifugal force

$l =$ length of transition curve.

We know that

$$P = \frac{mv^2}{R}$$

for constant mass & velocity of vehicle

$$P \propto \frac{1}{R} \quad \text{---} \quad \textcircled{1}$$

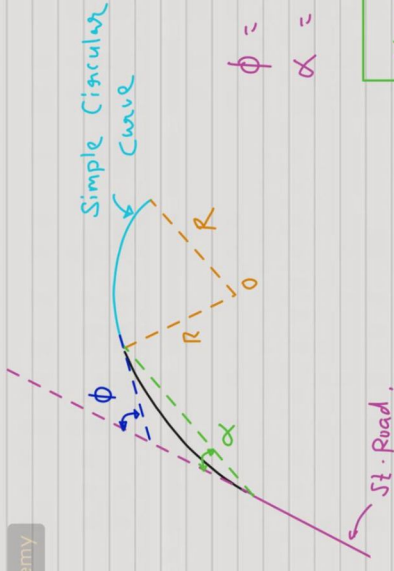
from eq. ① & ②

$$l \propto \frac{1}{R}$$

$$l = \frac{\text{Constant}}{R}$$

$$lR = \text{Constant}$$

This is fundamental condition of Ideal Transition Curve,
Euler Spinal, Clothoid & Glover Spinal Curve.



ϕ = Spinal angle

α = pole Deflection angle

$$\alpha = \frac{\phi}{3}$$

property of Ideal Transition Curve.

Equation of Curve in the form of Cartesian Coordinate.

- ① Euler spinal
- ② Cubic Spinal
- ③ Cubic parabola
- ④ Lamniscate Curve

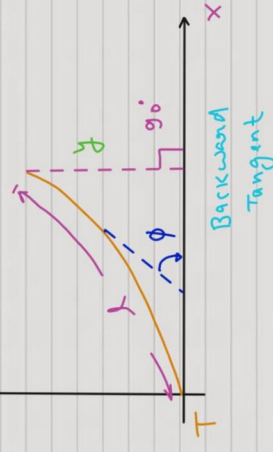
→ Cubic Spinal Curve ⇒

Assumption

$$\sin \phi = \phi$$

$$y = \frac{l^3}{6Rl} \quad \text{---} \quad \text{Equation of T.C.}$$

ϕ = Spinal angle.



l = Total length of T.C.

R = Radius of Simple Circular Curve

l = Distance of any point on T.C from Initial point (T)